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Research article

Mixed traffic flow of human-driven vehicles and connected autonomous vehicles: String stability and fundamental diagram

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Abstract: The introduction of connected autonomous vehicles (CAVs) gives rise to mixed traffic flow on the roadway, and the coexistence of human-driven vehicles (HVs) and CAVs may last for several decades. CAVs are expected to improve the efficiency of mixed traffic flow. In this paper, the carfollowing behavior of HVs is modeled by the intelligent driver model (IDM) based on actual trajectory data. The cooperative adaptive cruise control (CACC) model from the PATH laboratory is adopted for the car-following model of CAVs. The string stability of mixed traffic flow is analyzed for different market penetration rates of CAVs, showing that CAVs can effectively prevent stop-and-go waves from forming and propagating. In addition, the fundamental diagram is obtained from the equilibrium state, and the flow-density chart indicates that CAVs can improve the capacity of mixed traffic flow. Furthermore, the periodic boundary condition is designed for numerical simulation according to the infinite length platoon assumption in the analytical approach. The simulation results are consistent with the analytical solutions, suggesting the validity of the string stability and fundamental diagram analysis of mixed traffic flow.

Keywords: connected autonomous vehicle; human-driven vehicle; car-following; mixed traffic flow; heterogeneous traffic flow; string stability; fundamental diagram

1. Introduction

CAVs are designed to enhance mobility, safety, comfort and environmental sustainability, and this new technology will reshape the future transportation system [1]. Bansal and Kockelman [2] forecasted that the proportion of CAVs on the road would reach about 75% by 2050. There will be a transition period of several decades in which HVs and CAVs coexist on the roadway. CAVs inherently improve the characteristics of the mixed (HVs and CAVs) traffic flow, as the reaction delay and following time gap are effectively shortened [3–5].

CACC is one of the most promising technologies for CAVs [6,7], which is an extension of the

MBE, 20(2): 2280–2295. DOI: 10.3934/mbe.2023107 Received: 08 September 2022 Revised: 12 November 2022 Accepted: 13 November 2022 Published: 17 November 2022 adaptive cruise control (ACC) concept, sharing and receiving information such as location, velocity and acceleration. In recent years, numerous studies have confirmed that CAVs can stabilize the mixed traffic flow and increase roadway capacity. Back in 2008, Kesting et al. [8] proposed an improved ACC strategy and applied it to on-ramp bottleneck simulation, demonstrating that traffic congestion is alleviated when the proportion of ACC vehicles reaches 25%. Ngoduy [9] studied the stability diagram of the heterogeneous intelligent traffic flow under different ACC vehicle proportions applying the analytical stability framework [10] to the heterogeneous traffic flow of HVs and ACC vehicles. Ntousakis et al. [11] designed the traffic simulation experiments on a basic road section and a ring road, which shows that the traffic capacity can be significantly improved when the ACC penetration ratio is more prominent. Talebpour and Mahmassani [1] conducted string stability analysis and throughput analysis under different CACC/ACC vehicle ratios, which reveals that CAVs can improve string stability and be more effective in preventing shockwave formation and propagation. Chen et al. [12] proposed roadway capacity formulation for the mixed traffic flow, considering the influence factors such as market penetration of CAVs, the headway between CAV and the leading HV, and the driving rules. Liu et al. [13] studied the impact of CACC vehicles on the capacity of multi-lane expressways and conducted a case study on a 4-lane expressway with on and off ramps, showing that the traffic capacity increases slowly when the proportion of CACC vehicles ranges from 20% to 60%. Xie et al. [14] deduced a linear stability condition of the heterogeneous traffic with the generic car-following framework, demonstrating that the stability is closely related to the penetration rate and the spatial distribution of CAVs, particularly under congested traffic. Proving that the performance of CACC degrades to ACC when the CACC vehicle follows a manual-driven vehicle immediately in front, Wang et al. [15] investigated the stability of heterogeneous traffic flow analytically under various CACC market penetration rates. Yao et al. [16] developed the stability analysis method and fundamental diagram model of mixed traffic flow and conducted an on-ramp simulation with different CACC penetration rates. Yao et al. [17] conducted stability analysis and safety evaluation of mixed traffic flow under different penetration rates of CAVs, demonstrating the improvement of the stability and safety with CAVs application. Shang and Stern [18] simulated mixed traffic flow, finding out that bottleneck capacity is mainly affected by string stability and time gap, while downstream throughput is only affected by the time gap. Yao et al. [19] and Luo et al. [20] analyzed the linear stability of mixed traffic flow based on several influencing factors, including reaction time, the degradations of CAVs, and platoon intensity. Hung and Zhang [21] studied the effect of CACC on string stability for heterogeneous traffic with HVs, connected vehicles and autonomous vehicles. Liu et al. [22] focused on longitudinal platoon and conducted string stability analysis with numerical simulations, providing a new result about CACC with adaptive disturbance decoupling. Liu et al. [23] extended the standard string stability to head-to-tail string stability to explore the interaction of automated and human-driven vehicles in mixed platoons. Yao et al. [24] explored the fundamental diagram and linear stability of mixed traffic flow with the consideration of platoon size and intensity of CAVs.

Although various studies have been dedicated to the impact of CAVs on mixed traffic flow, twofold issues are open to discussion. First, most studies investigate HVs behavior with the model parameters from the literature [13–17,19–21,24], ignoring calibrating the model from the empirical dataset. Second, the open boundary conditions such as single-lane and on-ramp are frequently established scenarios for numerical simulations [1, 13, 15–18, 20], which may not coincide with the platoon of infinite vehicles concept in the analytical stability framework.

To overcome the above limitations, we investigate the car-following models of HVs and CAVs and conduct the string stability and fundamental diagram analysis of mixed traffic flow with analytical and numerical approaches. The contribution of this paper is summarized as follows: (i) HVs and CAVs are modeled based on the actual trajectory data, as they will interact in the real mixed traffic flow circumstance rather than in a simulation environment. The car-following behavior of HVs is modeled by the IDM and calibrated with the empirical dataset from a US highway. The CACC model from the PATH laboratory is based on the actual measured responses and adopted for CAVs modeling. (ii) The string stability and fundamental diagram are analytically investigated for different CAVs penetration rates, demonstrating that CAVs can effectively improve the stability and capacity of mixed traffic flow. (iii) The periodic boundary condition is introduced for numerical simulation, which is consistent with the assumption in the analytical process. The numerical simulation results agree with the analytical solutions, which proves the validity of the mixed traffic flow analysis framework.

The rest of the paper is structured as follows. In Section 2, the empirical dataset is prepared and used to calibrate HVs car-following model, and the CAVs car-following model is presented. In Section 3, we deduce the analytical solution of string stability and the fundamental diagram of mixed traffic flow. Section 4 establishes the numerical simulation in a ring road scenario and the simulation results are analyzed. Section 5 concludes our findings.

2. Microscopic traffic models

2.1. Data preparation

The driving behavior modeling of HVs plays an important role in mixed traffic flow analysis. The study of HVs requires the investigation of empirical data sources besides mathematical modeling. The next-generation simulation (NGSIM) dataset [25] is a frequently-used empirical dataset well known for its high-fidelity trajectory data extracted from high-angle shot videos. The data used here is part of the NGSIM dataset, i.e., the I-80 dataset, collected from eastbound/northbound US Interstate 80 (I-80) in Emeryville, California. The sampling area comprises six lanes (one high-occupancy vehicle lane and five regular lanes) and one on-ramp, approximately 500 m. The sampling period ranged from 4:00 p.m. to 4:15 p.m. on June 15, 2005.

First, we pick up trajectory data only collected from the regular inner lanes, Lanes 2–6, to avoid the impact of the on-ramp. Then, as in similar studies for the NGSIM data reconstruction [26–28], we filtered the trajectories to eliminate the measurement errors. Finally, 1386 car-following events are extracted by applying the three rules below:

- Gap distance less than 120 m, avoiding free-flow traffic conditions.
- Vehicle length less than 5 m, excluding truck.
- Car-following duration of no less than 30 s continuously, eliminating the influence of lane-changing.

The trajectories from Lanes 3–6 (1054 car-following events) are adopted to calibrate the HVs model, and the rest samples are from Lane 2 (332 car-following events) and further utilized for validation. Figure 1 shows a part of the trajectories in Lane 2.



Figure 1. Time-space diagram of some trajectories in Lane 2.

2.2. Car-following models

Car-following modeling is a way to explore the driving behavior of HVs and CAVs. In addition to being a microscopic traffic model, the car-following model is a bridge between micro and macro traffic flow analysis. Car-following models have been extensively studied over decades. There are many models developed for HVs incorporating human factors [29], which can be mainly divided into two categories: mathematical models (including stimulus-response models, desired measures models, psycho-physical models and Newell's simplified models) and data-driven models. As autonomous driving is a hot topic in recent years, some prevalent car-following models for CAVs are developed, such as the ACC and CACC models [30, 31] and reinforcement learning-based models [32, 33]. With a view to solving micromodels analytically, mathematics-based models are investigated in the following.

2.2.1. Human-driven vehicles

The IDM was first proposed in 2000, accurately reproducing phase transitions at road inhomogeneities [34]. This model can capture car-following behaviors of HVs, and its parameters have clear physical meanings. The governing equation of IDM is presented in Eq (2.1).

$$\dot{\nu} = a \left[1 - \left(\frac{\nu}{\nu_0}\right)^4 - \left(\frac{s^*(\nu, \Delta\nu)}{h-l}\right)^2 \right],\tag{2.1}$$

where \dot{v} is the derivative of speed, which denotes the acceleration of the subject vehicle. v is the speed of the subject vehicle. Δv is the relative speed, $\Delta v = v_{n-1} - v_n$, i.e., it can be calculated by the speed of the preceding vehicle minus the speed of the subject vehicle. h is the space headway between adjacent vehicles. l is the length of the preceding vehicle and set as 5 m. s^* is the desired space headway function, as given in Eq (2.2).

$$s^*(v,\Delta v) = s_0 + \max\left(0, Tv - \frac{v\Delta v}{2\sqrt{ab}}\right),\tag{2.2}$$

where the parameters to be calibrated are described as follows. *a* is the maximum acceleration, and *b* is the desired deceleration. v_0 denotes the desired speed. *T* is the safe time headway. s_0 is the

bumper-to-bumper space in standstill traffic, i.e., the minimum safe gap distance.

Since we intend to investigate HVs behavior at the real trajectory level, IDM parameters are calibrated based on a genetic algorithm (GA) [35] with prepared data. GA is a stochastic global search optimization algorithm. The optimization with respect to spacing is preferred [36], and the vehicle position can be calculated with the improved euler method, as in Eq (2.3). The optimization objective is the error between the simulated and observed trajectory, and the mean squared error (MSE) is used as the objective function in this study, as formulated in Eq (2.4). We conducted GA calibration with Python, and the parameter constraints are displayed in Table 1. The optimum set of calibrated parameters is presented in Table 2, and the values of these parameters from previous studies [34, 37, 38] are also listed. The IDM models with different parameters are validated and the average MSE results (i.e., $\overline{MSE} = 33.80, 31.29, 28.72$ and 26.89) show that the performance of calibrated parameters.

$$x_{t+\Delta t} = x_t + v_t \Delta t + \frac{1}{2} \dot{v}_{t+\Delta t} \Delta t^2, \qquad (2.3)$$

MSE =
$$\frac{1}{M} \sum_{t=1}^{M} (x_t^{sim} - x_t^{obs})^2$$
. (2.4)

Table 1. Parameter constrains for calibration [39].

Parameter	Bound	
$a(m/s^2)$	[0.1, 4.0]	
$b(m/s^2)$	[0.1, 4.5]	
$v_0 (km/h)$	[1, 150]	
T(s)	[0.1, 4.0]	
$s_0(m)$	[1.0, 10]	

Table 2. Parameters and measure of performance.

Source	$a (m/s^2)$	$b(m/s^2)$	$v_0 (km/h)$	T(s)	$s_0(m)$	MSE
[34]	0.73	1.67	120	1.6	2	33.80
[37]	1	1.5	128	1.1	2	31.29
[38]	1.4	2.0	120	1.5	2	28.72
Calibrated	1.71	2.02	95.36	1.32	2.87	26.89

2.2.2. Connected autonomous vehicles

PATH laboratory developed control models of ACC and CACC based on real vehicle implementation [30, 31], showing that the strings of ACC vehicles exhibit an unstable phenomenon, while CACC strings provide smooth and stable following action. In this paper, we focus on CAVs equipped with communication technology, which is conducive to the stability of mixed traffic flow. The CACC model derived from actual trajectories [31] is adopted to model CAVs, as formulated in Eq (2.5).

$$\begin{cases} e = h - l - s_0 - t_c v, \\ v = v_p + k_p e + k_d \dot{e}, \end{cases}$$
(2.5)

where *e* is the gap error between the actual and desired gap, this error and its derivative are used to determine the speed of the subject vehicle at each control cycle. t_c is the desired constant time gap, i.e., the expected traveling time for the subject vehicle with the instantaneous speed to the position of the rear end of the preceding vehicle. v_p is the speed of the subject vehicle at the previous control time. The control parameters k_p and k_d are used to adjust the time-gap error.

The control equation of the CACC model is obtained by calculating the derivative of speed in Eq (2.5), and the result is given in Eq (2.6).

$$\dot{v} = \frac{k_p(h - l - s_0) - k_p t_c v + k_d \Delta v}{k_d t_c + dt},$$
(2.6)

where *dt* is the updated time interval. The values of k_p , k_d and *dt* are determined by the experimental tests [31], $k_p = 0.45$, $k_d = 0.25$, dt = 0.01s. According to the investigation in [40], the acceptance value of t_c are different, and the maximum acceptance rate is 57% with $t_c = 0.6$.

3. Analytical solution of mixed traffic flow

3.1. String stability

There are two types of linear stability for car-following models, local stability and string stability [41,42], and the latter has received extensive attention in recent years, especially for the stability analysis of mixed traffic flow [1, 14, 16]. String stability is defined based on the phenomenon that fluctuations in the motion of one vehicle propagate to upstream traffic [43], and string instability gives rise to stop-and-go waves. This section investigates the string stability of mixed traffic flow of HVs and CAVs, guided by the method in previous studies [1, 10].

The car-following model for either HVs (Eq (2.1)) or CAVs (Eq (2.6)) can be simply expressed by the following differential equation, as in Eq (3.1). Under equilibrium points, the acceleration and relative speed in the above equation are zero ($\dot{v} = 0$ and $\Delta v = 0$), and there is an equilibrium solution for speed and gap distance ($v = v^e$ and $h = h^e$). Thus, Eq (3.2) presents the differential equation in the stable situation.

$$\dot{v} = f(v, \Delta v, h), \tag{3.1}$$

$$f(v^e, 0, h^e) = 0. (3.2)$$

Assuming small perturbations in headway and speed of a vehicle in an infinite-length platoon, Ward [10] deduced instability conditions for homogeneous and heterogeneous traffic flow, as shown in Eqs (3.3) and (3.4).

$$\frac{1}{2}(f_{\nu})^{2} - f_{\Delta\nu}f_{\nu} - f_{h} < 0, \qquad (3.3)$$

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$$\sum_{n} \left[\frac{1}{2} (f_{\nu}^{n})^{2} - f_{\Delta\nu}^{n} f_{\nu}^{n} - f_{h}^{n} \right] \left(\prod_{m \neq n} f_{h}^{m} \right)^{2} < 0,$$
(3.4)

where *n* and *m* denote different vehicle types in mixed traffic flow. f_{ν} , $f_{\Delta\nu}$, f_h are the partial differential of the car-following equation for speed, relative speed and headway, which are expanded as in Eq (3.5).

$$\begin{cases} f_{v}^{n} = \frac{\partial f(v, \Delta v, h)}{\partial v} \Big|_{(v^{e}, 0, h^{e})}, \\ f_{\Delta v}^{n} = \frac{\partial f(v, \Delta v, h)}{\partial \Delta v} \Big|_{(v^{e}, 0, h^{e})}, \\ f_{h}^{n} = \frac{\partial f(v, \Delta v, h)}{\partial h} \Big|_{(v^{e}, 0, h^{e})}. \end{cases}$$
(3.5)

Following this, the partial differential equations for car-following models of HVs and CAVs can be calculated, as shown in Eqs (3.6) and (3.7), where *H* and *C* denote HVs and CAVs, respectively. The parameters here are calibrated in the above section.

$$\begin{aligned}
f_{\nu}^{H} &= -2a \left[\frac{2}{v_{0}} \left(\frac{v^{e}}{v_{0}} \right)^{3} + \frac{T(s_{0} + Tv^{e})}{(h^{e} - l)^{2}} \right], \\
f_{\Delta\nu}^{H} &= \sqrt{\frac{a v^{e}(s_{0} + Tv^{e})}{b}}{\frac{b (h^{e} - l)^{2}}{(h^{e} - l)^{2}}}, \\
f_{h}^{H} &= 2a \frac{(s_{0} + Tv^{e})^{2}}{(h^{e} - l)^{3}}; \\
\begin{cases}
f_{\nu}^{C} &= -\frac{k_{p} t_{c}}{k_{d} t_{c} + dt}, \\
f_{\Delta\nu}^{C} &= \frac{k_{d}}{k_{d} t_{c} + dt}, \\
f_{h}^{C} &= \frac{k_{p}}{k_{d} t_{c} + dt}.
\end{aligned}$$
(3.6)
$$(3.7)$$

According to previous studies [1, 14, 44], for the mixed traffic flow of a platoon with infinite length, the judgment equation for string stability (Eq (3.4)) is related to the proportion of different vehicle types but independent of the distribution of vehicles. Therefore, assuming the penetration rate of CAVs in mixed traffic flow is p (0), the instability condition of mixed traffic flow can be written as in Eq (3.8). When <math>p is 0 or 1, the traffic flow is homogeneous. If p = 0, the platoon only contains HVs, and if p = 1, there are only CAVs. For these circumstances, the string stability is judged by Eq (3.3) with the corresponding differential equations.

$$(1-p)\left[\frac{1}{2}(f_{\nu}^{H})^{2} - f_{\Delta\nu}^{H}f_{\nu}^{H} - f_{h}^{H}\right] \times (f_{h}^{C})^{2} + p\left[\frac{1}{2}(f_{\nu}^{C})^{2} - f_{\Delta\nu}^{C}f_{\nu}^{C} - f_{h}^{C}\right] \times (f_{h}^{H})^{2} < 0.$$
(3.8)

Figure 2 depicts the string stability discrimination values in terms of different CAVs penetration rates (p). The result reveals that a higher penetration rate of CAVs improves the string stability of mixed traffic flow and increases the space headway threshold in which traffic becomes unstable. The red line

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in Figure 2 suggests that when the market penetration rate of CAVs is above 60%, the mixed traffic flow with any space headway stays stable. In particular, the discriminate values for 100% CAVs are constantly equal to 1.25, which indicates that the CAVs traffic flow is inherently stable in any circumstance.



Figure 2. String stability for different CAVs penetration rates.

3.2. Fundamental diagram

Fundamental diagram can be obtained by analyzing microscopic traffic model. At the equilibrium state, the acceleration of vehicles and the relative speed between vehicles are both zeros. By substituting them into Eqs (2.1) and (2.6), the steady space headway can be expressed by vehicle speed, as follows:

$$h^{eH} = \frac{s_0 + v^e T}{\sqrt{1 - (\frac{v^e}{v_0})^4}} + l,$$
(3.9)

$$h^{eC} = t_c v^e + l + s_0, ag{3.10}$$

where h^{eH} and h^{eC} denote steady space headway of HVs platoon and CAVs platoon, respectively.

We assume that a platoon of N vehicles travels at an equilibrium speed v^e , $v^e \in [0, v_0)$. With respect to CAVs penetration rate p, N(1-p) HVs and Np CAVs comprise the mixed traffic flow, which have different equilibrium space headway, h^{eH} and h^{eC} , respectively. The number of vehicles N is large enough to ignore the influence of the space headway of the first vehicle and the vehicle length of the last one. Hence, the mixed traffic flow covered road length L is the sum of the space headway of all vehicles at the equilibrium state, as formulated in Eq (3.11).

$$L = N(1 - p)h^{eH} + Nph^{eC}.$$
 (3.11)

According to the reciprocal relationship between density and space headway at an equilibrium state, the density of mixed traffic flow at the macroscopic level can be calculated by combining Eqs (3.9)–(3.11). Then, the flow at the macroscopic level is obtained based on the relationship between flow, density, and speed. Equation (3.12) presents the flow-density equation. Figure 3 provides the flow-density analytical curves of the fundamental diagram at different CAVs penetration rates p, $p \in \{0, 0.2, 0.4, 0.6, 0.8, 1\}$. A comparison of the analytical curves reveals that, for the same density, the traffic capacity is more significant when the penetration rate is higher. Moreover, when the penetration rate of CAVs is 100%, the maximum flow is 3935 veh/h, which is more than 2 times the maximum capacity of 100% HVs traffic flow. The results confirm that the growth of CAVs' market penetration rate is conducive to the efficiency of mixed traffic flow.

$$\begin{cases} k = \left[(1-p) \left(\frac{s_0 + v^e T}{\sqrt{1 - \left(\frac{v^e}{v_0} \right)}} + l \right) + p(t_c v^e + l + s_0) \right]^{-1}, \\ q = k v^e. \end{cases}$$
(3.12)



Figure 3. Fundamental diagram for different CAVs penetration rates.

4. Numerical simulation of mixed traffic flow

4.1. Simulation design

Numerical simulation is conducted to validate the analytical investigation for the stability and capacity of mixed traffic flow. The periodic boundary condition is an important experimental method in studying traffic flow stability [45]. The simulated vehicles run on a ring road without ramps, which can display the propagation course of disturbance in the platoon. This ring road condition is consistent with the infinite length platoon concept for the analytical solution, and it is supported by [46] that the policy studied in a closed network can be successfully applied to open networks.

The schematic of ring road is shown in Figure 4. There are 20 vehicles in the platoon, and the penetration rates of CAVs are set as 0, 20, 40, 60, 80 and 100%, which present the gradual commercialization of CAVs and the transition of mixed traffic flow. The positions of CAVs are randomly arranged in the platoon, as the schematic of 20% CAVs is shown in Figure 4. In the initial state, the vehicle travels at a steady-state speed and spacing, with a speed of 15.3 m/s. The steady spacing of HVs and CAVs can be calculated by Eqs (3.9) and (3.10), as 29.47 m and 17.05 m, respectively. Thus, for different CAVs penetration rates, the length of the ring road is variable, ranging from 341.0 m to 589.4 m. At 50 s, a perturbation is imposed on the first vehicle. This vehicle decelerates at a rate of 0.65 m/s² until its speed equals 14.0 m/s. Then it follows the vehicle immediately in front of it based on the car-following strategy. The entire simulation time is 200 s.



Figure 4. Schematic 20% CAVs penetration.

4.2. String stability

String stability of the traffic flow can be observed from the trajectory of vehicles. Based on the numerical simulation, the trajectories with different CAVs penetration rates are obtained, as shown in the time-space diagrams in Figure 5. It shows that when the penetration rate of CAVs transits from 0% to 100%, the steady-state speed of vehicles increases and steady-state spacing decreases. In other words, the traffic flow becomes more efficient. From Figure 5(a), when there is no CAV in the platoon, the perturbation has a negative effect on string stability and results in oscillations (stop-and-go waves) in the upstream traffic flow. Further introducing CAVs into the platoon will improve the string stability of traffic flow. As shown in Figure 5(b)–(e), the trajectories become smooth over time, and the oscillations mitigate. When the platoon consists entirely of CAVs, the impact of the perturbation is short-lived, as presented in Figure 5(f). Therefore, increasing the market penetration rate of CAVs dampens the impact of perturbation on traffic flow and enhances string stability, which agrees with the analytical solution.



Figure 5. Time-space diagrams with different CAVs penetration rates.

4.3. Fundamental diagram

In the numerical simulation, two virtual detectors are arranged on the ring road, and their interval is 100 m. The detectors can count the flow-density values during traffic simulation, i.e., generate the scatter points for the fundamental diagram. For different CAVs penetration rates, the simulated fundamental diagrams are compared with the analytical ones, as shown in Figure 6. It shows that the simulated density-flow values distribute around the analytical curves. Although the scatters are not

accurately dropping on the curves, they are fluctuating in reasonable ranges around the curves. Due to the speed disturbance in the simulation test, it is difficult for the traffic flow to reach an absolute equilibrium state, so there are non-equilibrium scatter points in the scatter simulation results. Moreover, the maximum capacity in the scatter plots gradually grows with the increase in CAVs penetration rate. Therefore, the simulation results are consistent with the analytical results, which proves the validity of

the fundamental diagram analysis in mixed traffic flow.

Figure 6. Simulated fundamental diagrams with different CAVs penetration rates.

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5. Conclusions

CAVs will shape the future of the roadway transport system. As the only route to the completely CAVs environment, mixed traffic flow is composed of HVs and CAVs and is vital to research. The main purpose of this paper is to study the stability and efficiency of mixed traffic flow. The car-following behaviors of HV and CAV are modeled by real-trajectory-based IDM and PATH laboratory's CACC, respectively. By adopting the mathematical analysis framework, the analytical investigation of string stability and fundamental diagram of mixed traffic flow with different CAVs percentages is conducted. The periodic boundary condition for numerical simulation is established according to the infinite length platoon assumption in the analytical approach. The results show that CAVs can improve the string stability of mixed traffic flow and alleviate the formation and propagation of stop-and-go waves. The capacity increases gradually with the increase of CAVs penetration rate, indicating that CAVs can effectively improve traffic efficiency. From the numerical simulation analysis, the simulation results are consistent with the analytical solutions, which proves the rationality and effectiveness of the string stability and fundamental diagram analysis of mixed traffic flow.

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Conflict of interest

All authors declare that there is no conflicts of interest in this paper.

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