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Research article

Input-output scaling factors tuning of type-2 fuzzy PID controller using multi-objective optimization technique

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Abstract: The PID controller is a popular controller that is widely used in various industrial applications. On the other hand, the control problems in microgrids (MGs) are so challenging, because of natural disturbances such as wind speed changes, load variation, and changes in other sources. This paper proposes an input-output scaling factor tuning of interval type-2 fuzzy (IT2F) PID controller using a multi-objective optimization technique. The suggested controller is applied to an MG frequency regulation problem. In the introduced controller the effect of variations of renewable energies (REs) and other disturbances are taken into account, and the robustness is investigated. In the multi-objective scheme, some factors such as least overshoot, and minimum settling/rising time are considered. The simulations show that by considering the suitable adjustment the desired regulation accuracy is achieved, such that the frequency trajectory shows the desired overshoot, and settling/rising time.

Keywords: PID; self-structuring; fuzzy controller; type-2 fuzzy logic; overshoot; settling/rising time **Mathematics Subject Classification:** 93C42, 93C40

1. Introduction

1.1. General

The increasing use of fossil fuels has caused major problems such as global warming, climate change, and environmental pollution. Using renewable energy as a viable alternative for reducing fossil fuel consumption is of particular importance. Nowadays, the integration of renewable energies has created microgrid (MG) power systems. The existing perturbations due to changes in wind speed over time and solar radiation as well as load power changes challenge the proper utilization of renewable energy. Designing a suitable controller that can balance energy generation and consumption and eliminate frequency fluctuations is of particular importance for the proper use of renewable energy [6, 12].

PIDs are extensively utilized in the industrial process because of their simplicity and capability [27]. However, uncertainties, nonlinearities, and the control parameters' variation deteriorate their efficiency of them. So, fuzzy logic systems (FLSs) and artificial neural networks (ANNs) are developed. To tackle the problem of the tuning procedures, some evolutionary optimization methods like GA and PSO have been utilized to design PID [1]. In these optimization algorithms, the overshoot and settling time are usually defined as the objective function (OB) to obtain suitable values for the PID gains. Although these tuning methods can improve the efficiency of these linear and fixed structure controllers, they are susceptible to the uncertainties and nonlinearities existing in the plant. As FLSs provides the ability to model uncertainty and imprecision which exists in most of the controlled systems, they were exploited to tune the PID parameters in the online mode and according to the defined rules by the experts [20,32].

1.2. Literature review

In these works, which are famous for fuzzy gain scheduling PID (FGSPID) techniques, the tracking error and derivative of error are considered as the input variables of FLS, and the PID gains are extracted from FLSs. In FGSPIDs, the control command is produced by the PID controller in which its gains change adaptively. Another combination of FLS and PID controller to design a nonlinear fuzzy PID (FPID) is to use the rules to realize parameters. The scheme of the FPID, a nonlinear PID, is similar to the structure of the classic PID from the viewpoint of input/output (I/O) dynamics. Unlike the FGSPID approach, in the FPID controller can be constructed using different types of FLSs. Among them, type-1 (T1) FLSs (T1FLSs) are a kind of linguistic variable that only can characterize a specific degree of imprecision or ambiguity. Interval type-2 (IT2) FLSs (IT2FLSs) are developed from of T1FLSs that introduce the concepts of uncertainty and imprecision as intervals and more robust to uncertainties such as measurement noise [8, 30, 31].

The other important forms of representing FLSs, generalized type-2 (GT2) FLS (GT2FLSs), which are similar to IT2FLSs, also inherently deal with uncertainty. In a situation where instead of representing uncertainty through an area, it is represented by a volume. Compared to the IT2FLSs, this form of uncertainty representation, fundamentally, is much more resilient to noise. In the FPID control design approaches, the important matter is how to set the input scaling coefficients (ISC)s and output-scaling factor (OSF), and parameters of the fuzzy controller (FC). In [10], PSO scheme was used to optimize the T1FPID controller for frequency in a power plant and it was shown that the controller

provided more desirable dynamic responses with regard to settling time and undershoots/overshoots. To better handle the nonlinearities, the big bang-big crunc and GA optimization approaches have been applied to adjust the interval T2FPID controllers' parametres in [16, 25], respectively. Using the combination of gradient-descent algorithm and Lyapunov theory, the OSFs and consequent parameters of an interval T2FPID controller were tuned for frequency control of micro-grid system [21]. The interval T2FPID controller in [21] was extended to regulate the frequency deviation of a time-delayed power system using a Lyapunov-Krasovskii functional. A fractional order GT2FPID controller was proposed in [23] in which its parameters were tuned based on the trial-and-error method. In many control problems, the control designing is a multi-objective (MO) problem in which several objectives, including its overshoot-undershoot and rising-settling time, must be optimized simultaneously. In this design method, the OBs are defined separately but optimized simultaneously, and the obtained results can be discussed based on the values of these OBs. It is worth pointing out that in the above methods, weighted values of different OBs were aggregated that resulting in a single OB which should be optimized by achieving optimal parameters for the FPID controller [33].

FPIDs are widely used for frequency control problems [15, 34]. For example, a hybrid version of bat and fuzzy algorithms is employed in [15] to tune the PI for the load control (LFC) application. The controller is employed in the four-area power plant. It is shown that the presented controller is robust enough in case of facing uncertainties related to external disturbances. An optimal interval T2F-PID is employed by Yesil [25] for an LFC problem. Big Bang Big Crunch optimization algorithm is used to adjust the scaling factors of the designed control. The efficiency of the designed algorithm is represented by comparing its performance with that of FPID. An FPID is proposed by Sahu et al., for automatic control. A teaching-learning approach is suggested in order to optimize the FPID in [22]. A hybrid scheme of harmony and cuckoo search methods is suggested in [9] for balancing the FPID parameters for an LFC problem. A hybrid model of PID-fuzzy-PID is designed by Debnath et al. [4] for the LFC problem. The parameters of the presented model are optimized using a modified grey wolf optimization algorithm. The sensitivity is analyzed to study the robustness of the presented controller. A novel hybrid fuzzy PD-PI controller based on an improved version of the moth swarm algorithm is suggested in [14].

1.3. Contribution

- Unlike the other LFC systems, the suggested controller does not depend on the MG models.
- The suggested approach considers both transient and steady-state response.
- The multi-optimization scheme is faster, and it results in better LFC accuracy.
- The suggested type-2 fuzzy-based approach has better robustness against uncertainties.

1.4. Paper organization

The remainder of this study is as follows: In Section 2, MG is explained. The FPID and associated tuning approach is illustrated in Sections 3–5. Simulations are given in Section 6. Finally, the conclusion is given in Section 7.

2. System description

MG systems consist of locally distributed loads connected to the distributed energy source. As can be seen in Figure 1, the studied MG included a PV system (with P_{pv} output), photocell (with Ppc output), WT generator (with Pwtg output), battery, flywheel energy storage system (ESS) and loads. The power changes of the studied system in the jth area are described as follows [13]:

$$\Delta P_{j,tie} = \sum_{i=1,i\neq j}^{N} \Delta P_{i,tie} = \frac{2\pi}{s} \left[\sum_{i=1,i\neq j}^{N} T_{ji} \Delta \omega_j - \sum_{i=1,i\neq j}^{N} T_{ji} \Delta \omega_i \right].$$
(2.1)

In (2.1), $\Delta P_{j,tie}$ denotes power changes. $\Delta \omega$ and T_{ji} are frequency deviation and torque coefficient respectively. First assume that we have just 2 areas. So, by applying disturbance to the first area, and considering N = 2, the power changes between the tie line and first area are calculated as follows:

$$\Delta P_{1,tie} = \frac{2\pi}{s} \left[T_{12} \Delta \omega_1 - T_{12} \Delta \omega_2 \right]. \tag{2.2}$$

Considering a first-order model, $\Delta \omega_2$ is obtained as follows:

$$\Delta\omega_2 = \frac{\left(\sum_{j=1}^n \Delta P_{m2i} - \Delta P_{2,tie} - \Delta P_{2L}\right)}{D_2 + 2H_2 s}.$$
(2.3)

From the fact that $\Delta P_m = 0$ under no speed governing, and $\Delta P_{2L} = 0$, we have:

$$\Delta\omega_2 = \frac{-\Delta P_{2,tie}}{D_2 + 2H_2 s}.$$
(2.4)

Also, by ignoring $\Delta \omega_1$, we can rewrite (2.2) as:

$$\Delta P_{1,tie} = \frac{2\pi}{s} T_{12} \Delta \omega_1. \tag{2.5}$$

Now consider the general scheme, and apply disturbance to the ith area, then $\Delta P_{j,tie}$ is obtained, similarly, as follows:

$$\Delta P_{j,tie} = \frac{2\pi}{s} \sum_{i=1, i \neq j}^{N} T_{ji} \Delta \omega_j, \qquad (2.6)$$

$$\Delta\omega_j = \frac{\left(-\Delta P_{j,tie} - \Delta P_{jL}\right)}{D_j + 2H_j s}.$$
(2.7)

By substituting (2.7) into (2.6) and considering step perturbation in load as $\Delta P_{jL}(s) = \frac{\Delta P_{jL}}{s}$, $\Delta P_{j,tie}$ is expressed as follows:

$$\Delta P_{j,tie} = \frac{-2\pi\Delta P_{jL}\sum_{i=1,i\neq j}^{N} \frac{T_{ji}}{2H_j}}{s\left(s^2 + D_j/2H_j + 2\pi\sum_{i=1,i\neq j}^{N} \frac{T_{ji}}{2H_j}\right)}.$$
(2.8)

Moreover, RDR is defined as follows:

$$RDP_{j} = \delta \frac{-\frac{d^{2}\Delta P_{j,ite}}{dt^{2}}H_{j}}{\pi \sum_{i=1,i\neq j}^{N} T_{ji}},$$
(2.9)

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where d is between 0 and 1. Figure 2 indicates diagram of the studied system and dynamics of various units.



Figure 1. Control block diagram of system.



Figure 2. The general diagram of case-study MG for each area.

3. Fuzzy PID controller

PID controllers are used in a wide range of industrial plants regarding the good capability. Nevertheless, the performance of these linear controllers is worsened due to nonlinearities, uncertainties, and parameter variation in the plant. To obtain a better system efficiency over the conventional PID controller, FLSs have been attempted to combine with PID controllers in two ways: (i) FLS has been employed to adjust the PID coefficients in an online way. In this approach which is known as gain adjusting PID by the use of fuzz logic (FGSPID), the inputs for FLS are considered to be the closed-loop error and its derivative, and according to the defined rules, the FLS determines the PID gains instantaneously. In this approach, the linear PID produces the control command to the controlled system (ii) in the second approach, the fuzzy rules are used for establishing a nonlinear PID. This approach is known as the FPID controller. Considering I/O relations, an FPID is analogous to linear PID, except that the FPID is an appropriate method for nonlinear systems. The common block of the FPID is provided in Figure 3 [26]. The membership functions (MFs) for inputs are depicted in Figure 4. For each input, 3 MFs are considered. To design the MFs just the upper and lower bounds of signals are taken into account. The parameters of MFs can also be optimized [35].

In the diagram, *u* represents the controller applied to the controlled system, *e* is the regulation/tracking error, u_f is the output signal of FC, α/β are the OSFs, and K_1 and K_2 are the ISCs. The FPID output can be regarded as follows:

$$u(t) = \alpha u_f(t) + \beta \int_0^t u_f(t) dt.$$
(3.1)

In [26] it is shown that the I/O relation of the FPID controller, like the classical PID controller, has the integral, derivative and proportional terms considering that this controller has a nonlinear characteristic and, therefore, it has been successfully utilized in controlling nonlinear and uncertain systems [5]. As mentioned earlier, the FPID controller can be realized using T1FLSs, IT2FLSs, and GT2FLSs. Since GT2FLSs are much more resilient dealing with noise and uncertainties, in this study, the designed FPID controller has been realized using this type FC.

Since in this problem, we have a high level of uncertainties the T2FLSs are used. The T2FLSs can handle more levels of uncertainty. In this paper, a T2FLS determines the parameters of a PI as shown in Figure 3.



Figure 3. Block diagram of the FPID controller.



4. Formulation of the FPID controller design as a MO problem

As mentioned earlier, the proper adjustment of the FPID controller i.e., α , β , K_1 , and K_2 , can enhance the efficiency [36]. Evolutionary optimization methods such as PSO and GA are one of the common offline methods in adjusting these parameters. In these scenarios, the FPID parameters are evaluated in a feasible area of response until the defined lost function is reduced. For a step reference input, the value of peak overshoot/undershoot, rise time, and settling-time are some important specifications to describe the transient performance. Disturbance rejection can be identified by presenting the peak overshoot/undershoot and settling-time. In order to establish the mentioned steadystate and transient performances using the evolutionary optimization methods, the performance indices based on various functions of the error are desired. Common performance indices including an error function in $[0, \infty)$ have been presented as the integral

$$I = \int_0^\infty f_k(e(t))dt \tag{4.1}$$

where $f_k(.)$ can takes various forms of error such as error. For example, using absolute error and square error as performance index penalize large errors more heavily than small ones which provide a longer settling time. By considering (2) as an OB, it is not possible to optimize the closed-loop performance characteristics i.e., the value of maximum overshoot/undershoot, rising-time, and settling time, at the same time. The reason for this is that some of these objectives are in conflict with each other and improving one of them leads to making the other worthwhile. Therefore, considering the objectives to be optimized, the tuning procedure of the FPID controller parameters can be regarded as a MO optimization problem. In this optimization method, several conflicting goals must be optimized simultaneously. Reducing the amount of the rise time (or settling time) will certainly raise the value of the peak overshoot of an optimized design. So, for MO problems, there is not a single solution, but with one run, we achieve a group of solutions, which is a kind of trade-off between the goals that must be optimized. It should be noted that in this paper α , β , K_1 and K_2 are the decision variables (it can be represented by vector x) and the settling time $f_1(x)$ and the value of peak overshoot/undershoot ($f_2(x)$) are the two conflicting objectives (see Figure 5).

Based on the relative importance of each objective (f_1 and f_2), each point of this curve is a solution for the decision variables, i.e., α , β , K_1 and K_2 . For example, if point A with the decision variables (solution) x_A is chosen, it means that, from the solutions obtained in the Pareto front, the closed-loop

he maximum amount of settling time

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system with the lowest amount of overshoot/undershoot and the maximum amount of settling time has been preferred. If point B with the decision variables x_B is chosen for the controller parameters, an output system with the lowest values for both objectives can be achieved. According to the Pareto front and unlike the single objective optimization methods, it is clear that in the MO methods a set of responses (located in the Pareto front) is obtained in which the controller designer can select the appropriate parameters on the basis of the relative importance of the objectives.

To solve the MO problem, some approaches that essentially depend on PSO and GA techniques were introduced [17, 19]. For example, Non-dominated sorting GA (NSGA-II) [3] and Niched Pareto GA (NPGA) [24] algorithms are based on GA technique. Also, strength Pareto evolutionary algorithm (SPEA) [11], adaptive weighted PSO (AWPSO) [18] algorithms are based on the PSO technique.



Figure 5. Concept of Pareto front.

5. AWPSO algorithm for MO problem

The PSO is based on population search and it depends on the simulation of bird behavior. Some methods have been suggested to increase the accuracy of the basic PSO. One of these methods is the adaptive weighted PSO (AWPSO) algorithm; the velocity equation of the basic PSO algorithm in it is changed as follows (see the main general flowchart in Figure 6):

$$\vec{v}_i(t) = w\vec{v}_i(t-1) + \rho \left[c_1 r_1 \left(\vec{P}_{bi} - \vec{x}_i(t-1) \right) + c_2 r_2 \left(\vec{P}_g - \vec{x}_i(t-1) \right) \right]$$
(5.1)

where, $\vec{x_i}$ shows the position of P_i at t. In this algorithm, ρ is the acceleration variable as:

$$\rho = \rho_0 + \frac{t}{T}.\tag{5.2}$$

Defining an aggregate OB is examined as one of the straightforward methods to tackle the MO problems. To get optimum solutions, single objective optimization algorithms, without any revision

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to these algorithms, can then be utilized. An aggregation method is used to introduce the evaluation function, Eval, for MO problem as follows [7]:

$$\operatorname{Eval}(k) = \sum_{i=1}^{n} \theta_i f_i(k), \quad \sum_{i=1}^{n} \theta_i = 1$$
(5.3)

for k-th particle, *n* denotes number of OBs and θ_i denotes the related parameters for each OB. This Eval function can be normalized as follows:

$$\theta_i = \frac{\mu_i}{\sum_{i=1}^n \mu_i} \tag{5.4}$$

where μ_i and μ_j are uniform random numbers in the interval [0, 1].

Remark 1. To apply the AWPSO algorithm to our control problem, the various values for the parameters of suggested FPID are considered as the possible solution (population) of the AWPSO algorithm. Then, at each sample time, the best solution of AWPSO is considered as the coefficient of our controller.



Figure 6. The general flowchart.

6. Simulation results

The IEEE 39-bus test system (see Figure 7 [28]) is used to evaluate the efficiency of the presented controller for the fuzzy logic controller(FLC) under three different scenarios. The parameters are given in Table 1. The first column of Table 1 indicates the restrictions on the performance of output signals. For example, to have a minimum overshoot and maximum settling time, the values of parameters are

 $\alpha = 1.63$, $\beta = 0.186$, $K_1 = 2.98$, and $K_2 = 3.4$. The demand response (DR) was obtained as 98.77, 22.21, and 54.6 MW in the first, second and third areas, respectively. Two main scenarios have been discussed in this paper. In the first scenario, the effect of load changes is investigated, and in the second one, the effect of wind speed is examined.



Figure 7. IEEE 39-bus test system.

	0	ß	K.	K.
	u	p	N	R 2
Maximum	1.63	0.186	2.98	3.4
settling time,				
Minimum				
overshoot				
Mediocre	2.9	0.12	1.186	3.86
Minimum settling	2.66	0.109	0.86	4.28
time, Maximum				
overshoot				

Table 1. Simulation parameters.

The load changes are investigated as a disturbance. Figure 8 shows the load change considered in the study. We see that load is changed the time t=30 s, from 0 to 8 MV. It can be considered as a high disturbance. Figure 9 compares frequency regulation in the first, second and third areas with

other methods. Figure 9 shows that frequency changes tended to 0 in all three areas using the proposed method. The comparison condition for the suggested method, PI controller based on type-1 FLC (T1-FLC), and PI controller based on type-2 FLC (T2-FLC) [29] are the same. It means that the rules are the same for all three controllers.



Figure 9. Comparison of frequency changes for various controllers.

The results revealed performance of the suggested method was superior to other approaches. Furthermore, the effect of wind speed, which varies over time, on the performance of the controller in frequency regulation was investigated in this scenario. Figure 10 indicates the speed change diagram. We see that the wind speed is randomly changed, and it can be considered as a high perturbation. Figure 11 examines the proposed controller performance in frequency regulation. The proposed controller had good performance in resisting wind speed changes over time and was superior to other methods.

The results show that the suggested LFC adequately resists the uncertainties, such as wind speed changes, DR changes, and uncertain dynamics. The main reason is that the parameters of the PI are not fixed, but they are adaptively changed. Also, the suggested optimization scheme finds suitable rules for T2FLS.



Figure 11. Comparison of frequency changes for various controllers in presence of wind speed.

Remark 2. The primary focus of this study is on the LFC problem. But, the designed controller does not use dynamics and can be easily extended for other problems in MGs. Also, the suggested controller can be improved using new PIDs and fuzzy controllers [37–42].

7. Conclusions

The PIDs are widely used for load frequency control problems. But the main problem is their accuracy in the verses of high uncertainties. Also, in most of the existing studies, just the tracking error is considered, and the transient response is neglected. In this study, a novel technique to frequency control in MGs is proposed. A multi-objective optimization approach is proposed, as well as a novel PID controller. The developed controller is implemented in a case-study multi-area MG, and its performance is assessed under perturbations. In the first case, a rapid change in output load is examined, in addition to unknown dynamics. It is demonstrated that the proposed PID controller effectively manages perturbations and stabilizes the plant. The wind turbines are also supposed time-

varying in the second assessment, in addition to dynamic uncertainty and load fluctuations. The results, as well as comparisons with other FPID approachers, reveal that the introduced PID has satisfactory regulatory results. The main disadvantage of the suggested approach is the computation process of the optimization, which can be simplified for future studies.

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Conflict of interest

The authors declare no conflict of interest.

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